

## Tutorial

If  $\vec{B}$  is uniform show that  $\vec{A}(\vec{r}) = -\frac{1}{2}(\vec{r} \times \vec{B})$

The curl of  $\vec{A} = -(\vec{r} \times \vec{B})/2$  is equal to

$$\vec{\nabla} \times \vec{A} = -\frac{1}{2} \vec{\nabla} \times (\vec{r} \times \vec{B}) = -\frac{1}{2} \left[ (\vec{B} \cdot \vec{\nabla}) \vec{r} - (\vec{r} \cdot \vec{\nabla}) \vec{B} + \vec{r} (\vec{\nabla} \cdot \vec{B}) - \vec{B} (\vec{\nabla} \cdot \vec{r}) \right]$$

Since  $\vec{B}$  is uniform it is independent of  $x, y, z$ , therefore 2nd & 3rd term on RHS are 3-0.

The 1st term in Cartesian coordinates is equal to

$$\begin{aligned} (\vec{B} \cdot \vec{\nabla}) \vec{r} &= \left( B_x \frac{\partial}{\partial x} + B_y \frac{\partial}{\partial y} + B_z \frac{\partial}{\partial z} \right) (x\hat{i} + y\hat{j} + z\hat{k}) \\ &= B_x \hat{i} + B_y \hat{j} + B_z \hat{k} = \vec{B} \end{aligned}$$

The 4th term, in Cartesian

$$\vec{B} (\vec{\nabla} \cdot \vec{r}) = \vec{B} \left( \frac{\partial}{\partial x} x + \frac{\partial}{\partial y} y + \frac{\partial}{\partial z} z \right) = 3\vec{B}$$

Therefore, the curl of  $\vec{A}$  is equal to

$$\vec{\nabla} \times \vec{A} = -\frac{1}{2} (\vec{B} - 3\vec{B}) = \vec{B}$$

The divergence of  $\vec{A}$  is equal to

$$\vec{\nabla} \cdot \vec{A} = -\frac{1}{2} \vec{\nabla} \cdot (\vec{r} \times \vec{B}) = -\frac{1}{2} \left[ \vec{B} \cdot (\vec{\nabla} \times \vec{r}) - \vec{r} \cdot (\vec{\nabla} \times \vec{B}) \right] =$$

## Three Fundamental Quantities of Magnetostatics

The current density  $\vec{J}$

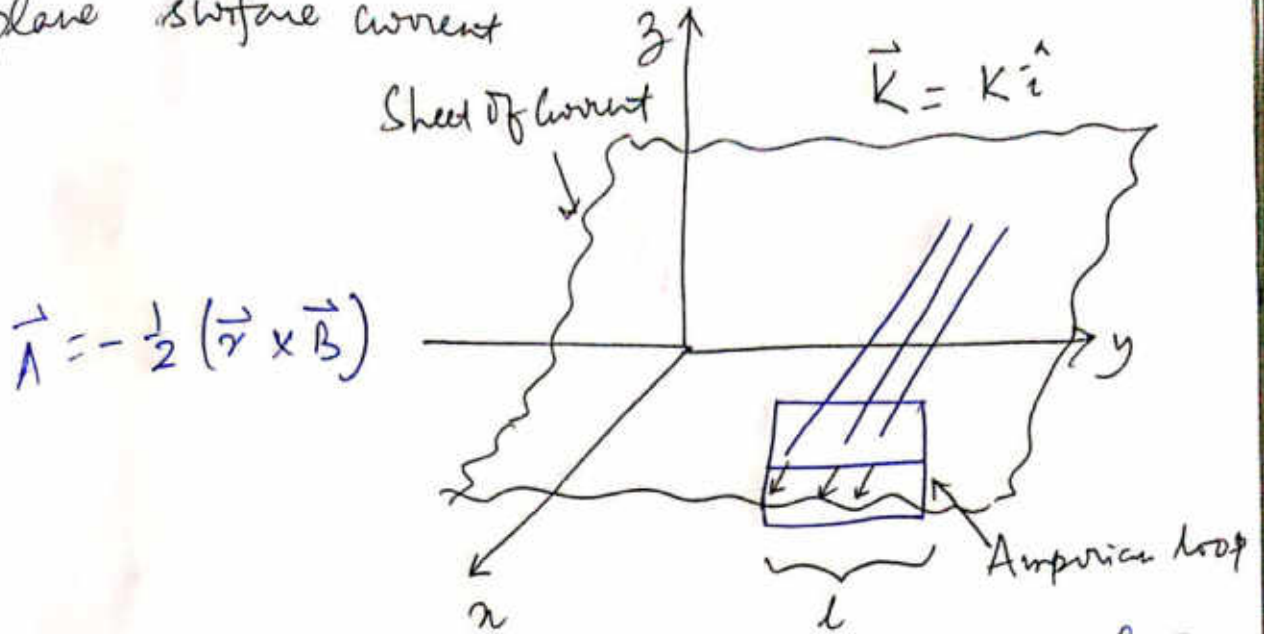
The mag field  $\vec{B}$

The vector potential  $\vec{A}$

If one of them is known the other two can be calculated.

Known $\downarrow$	$\vec{J} =$	$\vec{B} =$	$\vec{A} =$
$\vec{J}$		$\frac{\mu_0}{4\pi} \int \frac{\vec{J} \times \Delta \vec{r}}{\Delta r^2} d\tau$	$\frac{\mu_0}{4\pi} \int \frac{\vec{J}}{\Delta r} d\tau$
$\vec{B}$	$\frac{1}{\mu_0} (\nabla \times \vec{B})$		$\frac{1}{4\pi} \int \frac{\vec{B} \times \Delta \vec{r}}{\Delta r^2} d\tau$
$\vec{A}$	$-\frac{1}{\mu_0} \nabla^2 \vec{A}$	$\nabla \times \vec{A}$	

2. Find the vector potential above and below the plane surface current



Since the surface current extends to infinity we cannot use the surface integral of  $\vec{K}/\Delta r$  to calculate  $\vec{A}$  and an alternative method. In the region above the  $xy$  plane ( $z > 0$ ) the mag field is equal to

$$\vec{B} = -\frac{\mu_0}{2} K \hat{j}$$

Therefore,

$$\vec{A} = -\frac{1}{2} (\vec{r} \times \vec{B}) = -\frac{1}{2} \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ x & y & z \\ 0 & -\frac{\mu_0}{2} K & 0 \end{vmatrix}$$

$$= -\frac{\mu_0}{4} K z \hat{i} + \frac{\mu_0}{4} K x \hat{k}$$

In the region below the  $xy$  plane ( $z < 0$ ) the mag field

$$\vec{B} = \frac{\mu_0}{2} K \hat{j}$$

Therefore,

$$\vec{A} = -\frac{1}{2} (\vec{r} \times \vec{B}) = -\frac{1}{2} \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ x & y & z \\ 0 & \frac{\mu_0}{2} K & 0 \end{vmatrix} = \frac{\mu_0}{4} K z \hat{i} - \frac{\mu_0}{4} K x \hat{k}$$

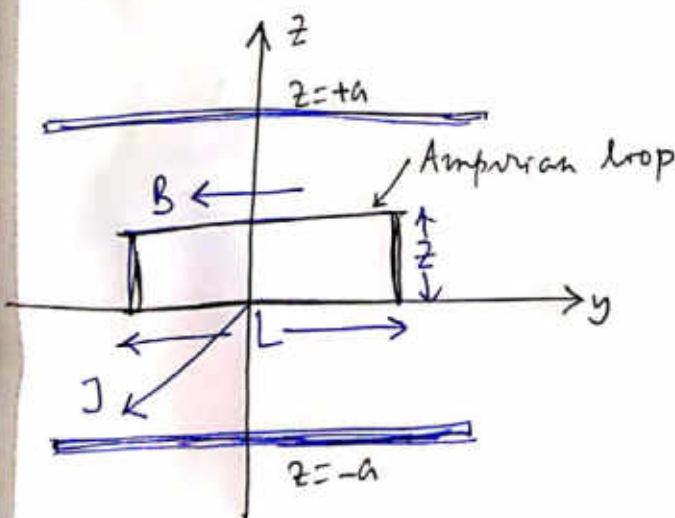
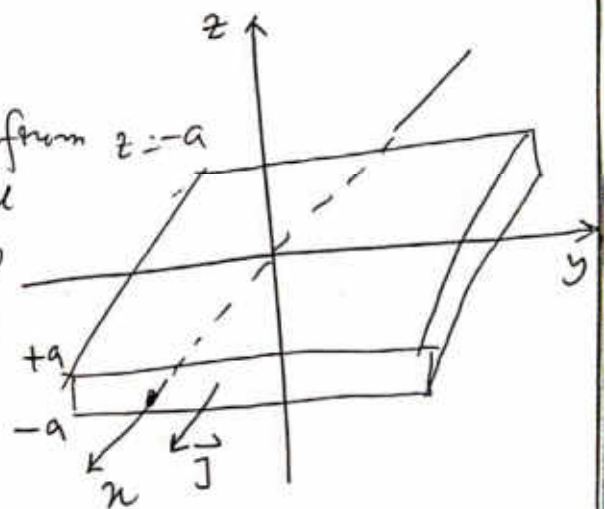
We can verify that by calculating  $\nabla \times \vec{A}$

For  $z > 0$ :

$$\nabla \times \vec{A} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -\frac{\mu_0 K_z}{4} & 0 & \frac{\mu_0 K_z}{4} \end{vmatrix} = -\frac{\mu_0}{2} K_z \hat{j} = \vec{B}$$

The vector potential  $\vec{A}$  is however not uniquely defined. For ex:  $\vec{A} = -\frac{\mu_0}{2} K_z \hat{i}$  and  $\vec{A} = \frac{\mu_0}{2} K_x \hat{k}$  are also possible  $\vec{A}$ 's that generate the same mag fld. These  $\vec{A}$ 's also satisfy the requirement that  $\nabla \cdot \vec{A} = 0$ .

3. A thick slab extending from  $z = -a$  to  $z = +a$  carries a uniform vol current  $\vec{J} = J \hat{i}$ . Find the mag fld as a f<sup>n</sup> of  $z$ , both inside and outside the slab.



Symmetry

mag fld  $z > 0$

⇓ mirror image

mag fld  $z < 0$

In the Amperian loop the mag fld = 0 in  $z = 0$  current is flowing out of the paper

dir<sup>n</sup> of  $d\vec{A}$  to be  $\parallel$  to the dir<sup>n</sup> of  $\vec{J}$

Therefore  $\int \vec{J} \cdot d\vec{a} = J_z L \quad 0 < z < a$

Surface

$$\int \vec{J} \cdot d\vec{a} = J_a L \quad z > a$$

Surface

The dir<sup>n</sup> of evaluation of the line integral of  $\vec{B}$  must be consistent with our choice of the dir<sup>n</sup> of  $d\vec{a}$  (right-hand rule). This requires that the line integral of  $\vec{B}$  not be evaluated in a counter-clockwise dir<sup>n</sup>. The line integral of  $\vec{B}$  is equal to

$$\oint \vec{B} \cdot d\vec{l} = B L$$

line

Applying Ampere's law we obtain  $B$ :

$$B = \frac{\mu_0}{L} \int \vec{J} \cdot d\vec{a} = \mu_0 J_z \quad 0 < z < a$$

Surface

$$B = \frac{\mu_0}{L} \int \vec{J} \cdot d\vec{a} = \mu_0 J_a \quad z > a$$

Surface

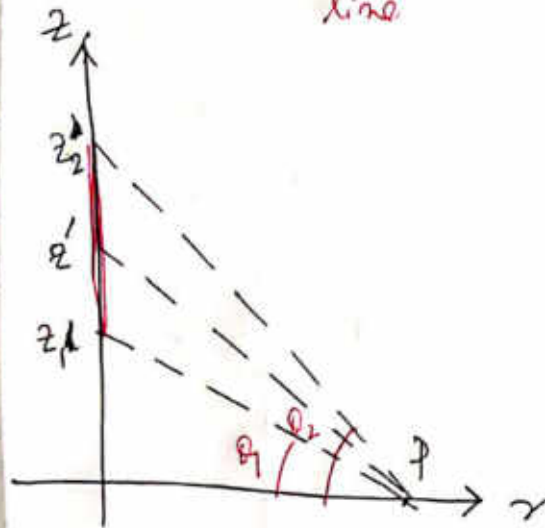
Thus  $B(z) = -\mu_0 J_a \hat{j} \quad a < z$

$$B(z) = -\mu_0 J_z \hat{j} \quad -a < z < a$$

$$B(z) = \mu_0 J_a \hat{j} \quad z < -a$$

4. Find the magnetic vector potential of a finite segment of straight wire, carrying a current  $I$ .

$$\vec{A} = \frac{\mu_0}{4\pi} \int_{\text{line}} \frac{\vec{I}}{r} dl = \frac{\mu_0 I}{4\pi} \int_{\text{line}} \frac{dl}{r} \text{ for line current}$$



The current at infinity is zero, therefore we can use the expression for  $\vec{A}$  in terms of the line integral of the current  $I$ . Consider the wire located along the  $z$ -axis between  $z_1$  and  $z_2$  and use cylindrical coordinates. The vector potential at a pt.  $P$  is independent of  $\phi$  (cylindrical symmetry) and equal to

$$\vec{A} = \frac{\mu_0}{4\pi} \int_{\text{line}} \frac{dl}{r} = \frac{\mu_0 I}{4\pi} \int_{z_1}^{z_2} \frac{dz'}{\sqrt{r^2 + z'^2}} \hat{k} = \frac{\mu_0 I}{4\pi} \ln \left[ \frac{z_2 + \sqrt{r^2 + z_2^2}}{z_1 + \sqrt{r^2 + z_1^2}} \right] \hat{k}$$

Here we have assumed that the origin of the coordinate system is chosen such that  $P$  has  $z=0$

$$\begin{aligned} \vec{B} = \nabla \times \vec{A} &= -\frac{\partial A_z}{\partial r} \hat{\phi} = -\frac{\mu_0 I}{4\pi} \left[ \frac{r}{\sqrt{r^2 + z_2^2}} \frac{1}{z_2 + \sqrt{r^2 + z_2^2}} - \frac{r}{\sqrt{r^2 + z_1^2}} \frac{1}{z_1 + \sqrt{r^2 + z_1^2}} \right] \hat{\phi} \\ &= \frac{\mu_0 I}{4\pi r} \left[ \frac{z_2}{\sqrt{r^2 + z_2^2}} - \frac{z_1}{\sqrt{r^2 + z_1^2}} \right] \hat{\phi} = \frac{\mu_0 I}{4\pi r} [\sin \theta_2 - \sin \theta_1] \hat{\phi} \end{aligned}$$